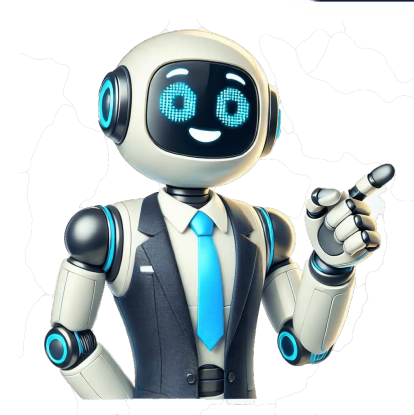


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[illegible]

/3) / M0 = 1441.9 kNVy,Ed / Vc,y,Rd = 0.235PASS Design shear resistance exceeds design shear forceCheck bending moment Section 6.2.5Design bending moment;My,Ed = 579.2 kNmDesign bending resistance moment eq 6.13;Mc,y,Rd = Mpl,y,Rd = Wpl,yfy / M0 = 1470 kNmMy,Ed / Mc,y,Rd = 0.394PASS Design bending resistance moment exceeds design bending momentCheck bending and axial force Section 6.2.9Bending and axial force check eq 6.33 & eq 6.34;Ny,lim = min(0.25Npl,Rd, 0.5hwtwfy / M0) = 1070.5 kNNEd / Ny,lim = 0.654Allowance need not be made for the effect of the axial force on the plastic resistance moment about the y-y axisBending and axial force check eq 6.35;Nz,lim = hwtwfy / M0 = 2141.0 kNNEd / Nz,lim = 0.427Allowance need not be made for the effect of the axial force on the plastic resistance moment about the z-z axisN = max(5n, 1) = 1For bi-axial bending eq 6.41;[My,Ed / Mpl,y,Rd]N + [Mz,Ed / Mpl,z,Rd]N = 0.171PASS Biaxial bending utilisation is acceptableCheck combined bending and compression Section 6.3.3Equivalent uniform moment factors Table B.3;Cmy = 1.000Cmz = 1.000CmLT = 1.000Interaction factors kij for members susceptible to torsional deformations Table B.2Characteristic moment resistance;My,Rk = Wpl,yfy = 1470 kNmCharacteristic moment resistance;Mz,Rk = Wpl,zfy = 303.1 kNmCharacteristic resistance to normal force;NRk = Afy = 6044.2 kNInteraction factors;kyy = Cmy(1 + min(y 0.2, 0.8) NEd / (yNRk / M1)) = 0.986kzy = min(0.6 + z, 1 0.1zNEd / ((CmLT 0.25) zNRk / M1)) = 0.991kzz = Cmz(1 + min(2z 0.6, 1.4) NEd / (zNRk / M1)) = 1.033kyz = 0.6kzz = 0.620Interaction formulae eq 6.61 & eq 6.62;NEd / (yNRk / M1) + kyyMy,Ed / (cLTMy,Rk / M1) + kyzMz,Ed / (Mz,Rk / M1) = 0.55NEd / (zNRk / M1) + kzyMy,Ed / (cLTMy,Rk / M1) + kzzMz,Ed / (Mz,Rk / M1) = 0.571PASS Combined bending and compression checks are satisfied.The result below depicts the internal stresses induced in the bottom chord at the load combination 1.35gk + 1.5qk (where qk represents the UDL component of the traffic load only).The result below depicts the internal stresses induced on the bottom chord under the unfactored moving tandem wheel load only.Design Axial compression : 1181.948 + 1.5(761.358) = 2324 kNDesign axial tension = 928.940 + 1.5(623.655) = 1864 kNDesign major bending moment: (ignored for brevity)Design minor axis bending moment = (ignored for brevity)Design Shear (major axis) = (ignored for brevity)Design Shear (minor axis) = (ignored for brevity)Classification of cross sections Section 5.5 = [235 N/mm2 / fy] = 0.92Internal compression parts subject to compression Table 5.2 (sheet 1 of 3)Width of section;c = b 3t = 212.5 mmc / t = 17 = 18.4

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